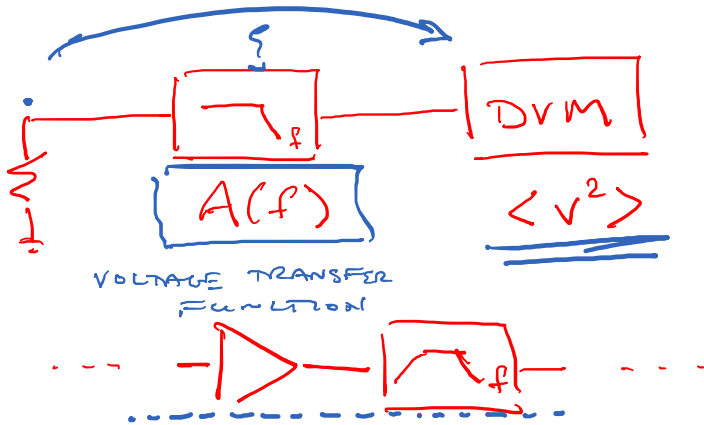


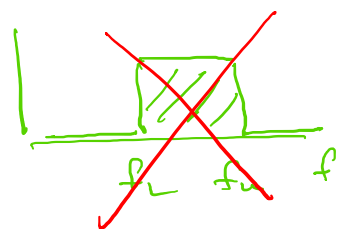
# NOISE BANDWIDTH REVISITED

$$S_v = 4k_B T R$$

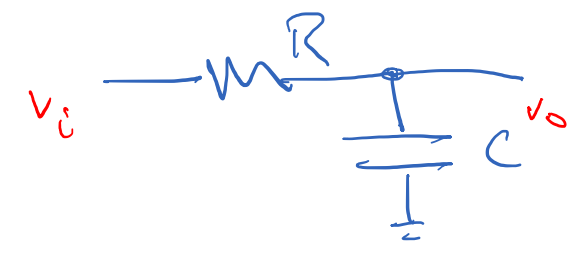
$R @ T$



"BRICK WALL" FILTER



e.g.



$$A = \frac{v_o}{v_i}$$

$$\tau = RC$$

$$\Delta f_N = \frac{1}{4RC}$$

NOISE BANDWIDTH.

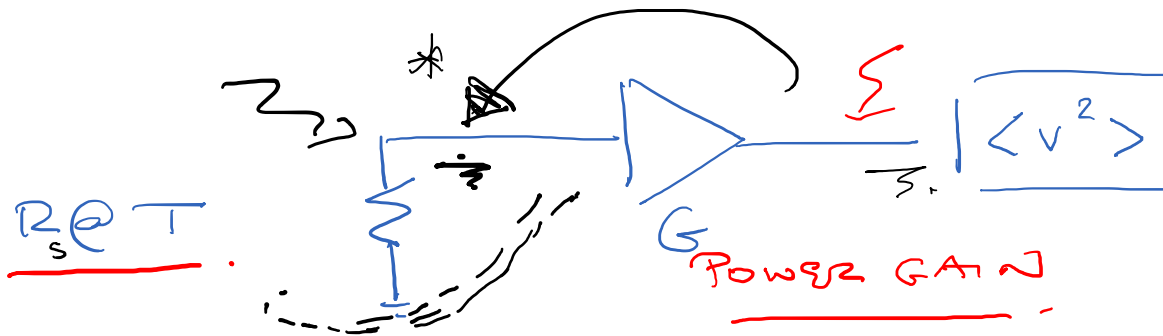
$$\Delta f_N = \int |A(f)|^2 df$$

$$\underline{\underline{\langle v^2 \rangle = 4k_B T R \Delta f_N}}$$

(COMPARE:

$$\Delta f_{3dB} = \frac{1}{2\pi RC})$$

# AMPLIFIER ADDS NOISE



$\delta x, \delta y$

TOTAL FLUCTUATION  
 $[\delta x^2 + \delta y^2]^{1/2}$

$$\sigma_z^2 = \sigma_x^2 + \sigma_y^2$$

ADDING NOISE  
 INCOHERENTLY

OUTPUT:  $\langle v^2 \rangle = G \left[ 4k_B T R_s \Delta f_N \right] + \text{NOISE [AMP]}$

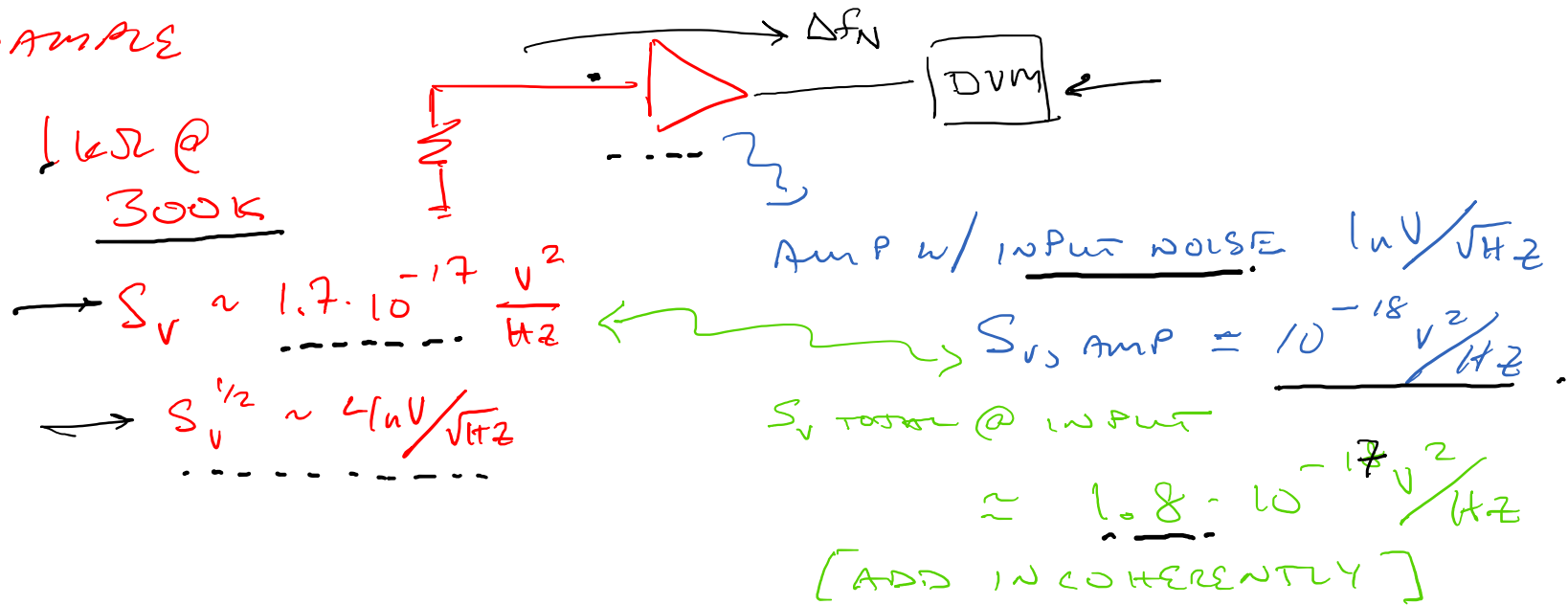
$$= G \left[ 4k_B T R_s \Delta f_N + \text{AMP INPUT NOISE} \right]$$

$$= G \left[ 4k_B R_s \Delta f_N \left( T + T_N \right) \right]$$

→ NOISE TEMPERATURE  $T_N$

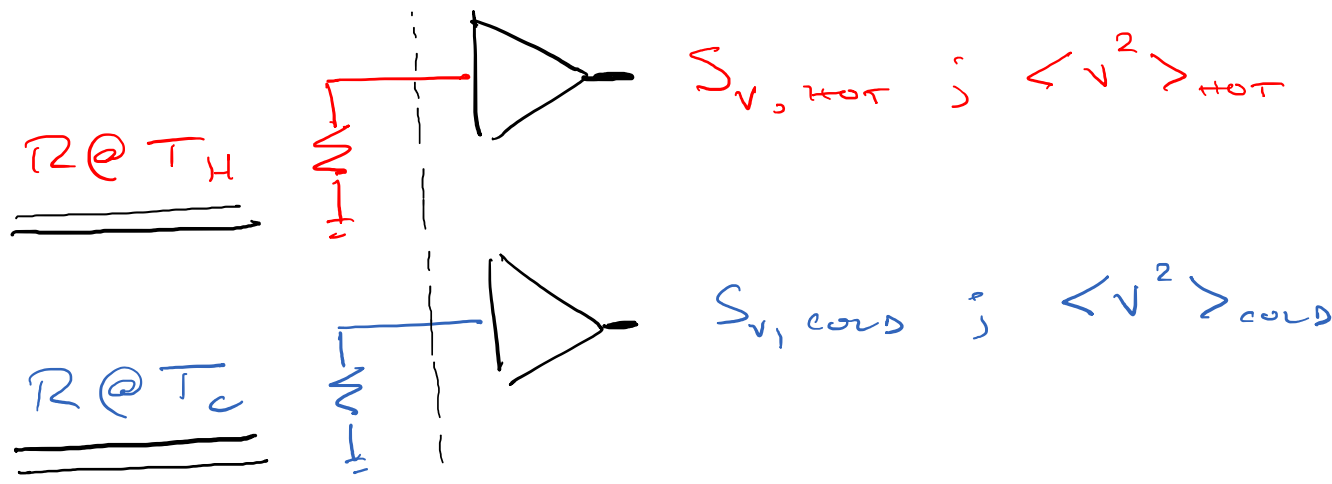
FUNCTION OF  $f_s$ ,  
 OF  $R_s$

EXAMPLE



$$T_N = \left( 300 \text{ K} \cdot \frac{10^{-18} \frac{\text{V}^2}{\text{Hz}}}{1.7 \cdot 10^{-17} \frac{\text{V}^2}{\text{Hz}}} \right) = 18 \text{ K}$$

HOT LOAD / COLD LOAD



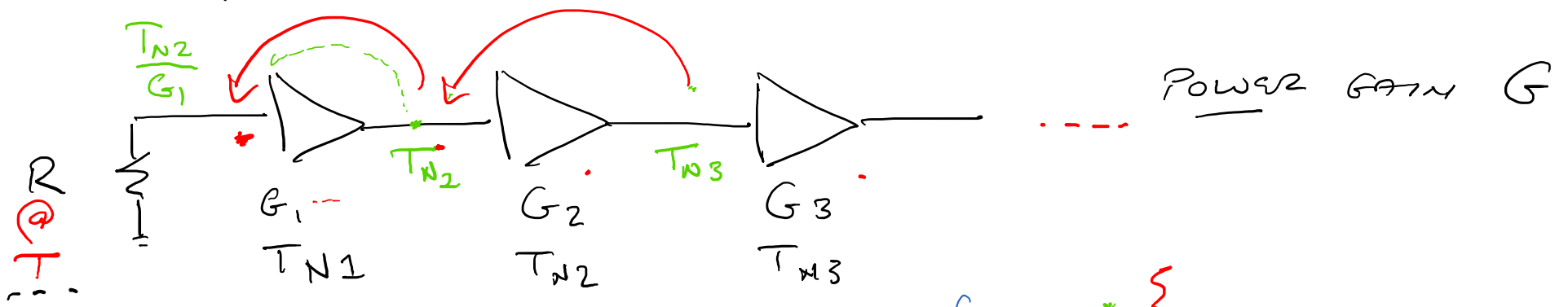
$$\frac{\langle v^2 \rangle_H}{\langle v^2 \rangle_C} = \frac{4k(T_H + T_N)R\Delta f}{4k(T_C + T_N)R\Delta f}$$

$$\frac{\langle v^2 \rangle_H}{\langle v^2 \rangle_C} = \frac{S_{v, HOT}}{S_{v, COLD}} = \frac{T_H + T_N}{T_C + T_N}$$

SELF-CALIBRATING

NOTE:  $T_x$  GENERALLY A FUNCTION OF FREQUENCY.

# $T_N$ OF CASCADED AMPLIFIERS



NOISE POWER @ OUTPUT  $\sim G_3 \left\{ G_2 \left[ G_1 (T + T_{N1}) + T_{N2} \right] + T_{N3} \right\}$

REFER TO INPUT

$$T_{N, \text{TOTAL}} = T_{N1} + \frac{T_{N2}}{G_1} + \frac{T_{N3}}{G_1 G_2} + \dots$$

# NOISE FIGURE

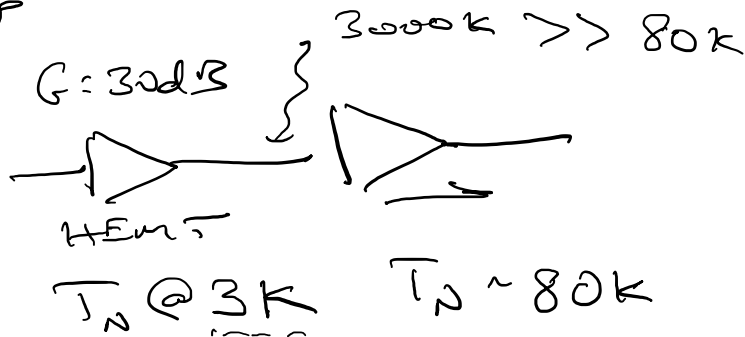
$$\rightarrow NF = 10 \log_{10} \left( \frac{T + T_{N1}}{T} \right) \quad \underline{T = 300K}$$

$$NF \sim 1 \text{ dB} \Leftrightarrow 80 \text{ K } T_{N1}$$

$$3 \text{ dB} \Leftrightarrow 300 \text{ K } T_{N1}$$

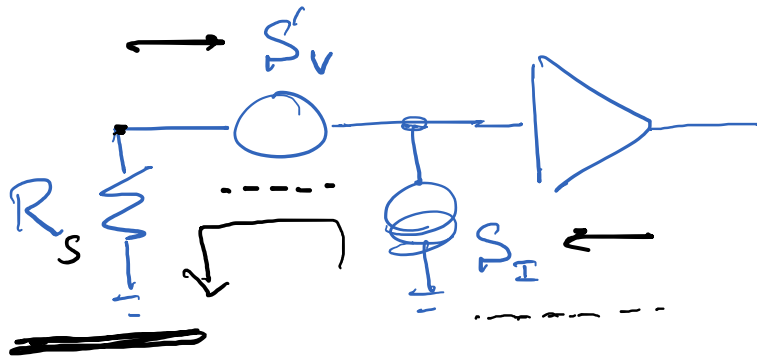
example

CASCADES  
AMP



$$T_{N, \text{total}} = 3K + \frac{80K}{10^3} \sim \underline{\underline{3.08K}}$$

# AMPLIFIER NOISE ... MORE DETAILS



$$S_v + S_i R^2 = 4k_B T_N R_s$$

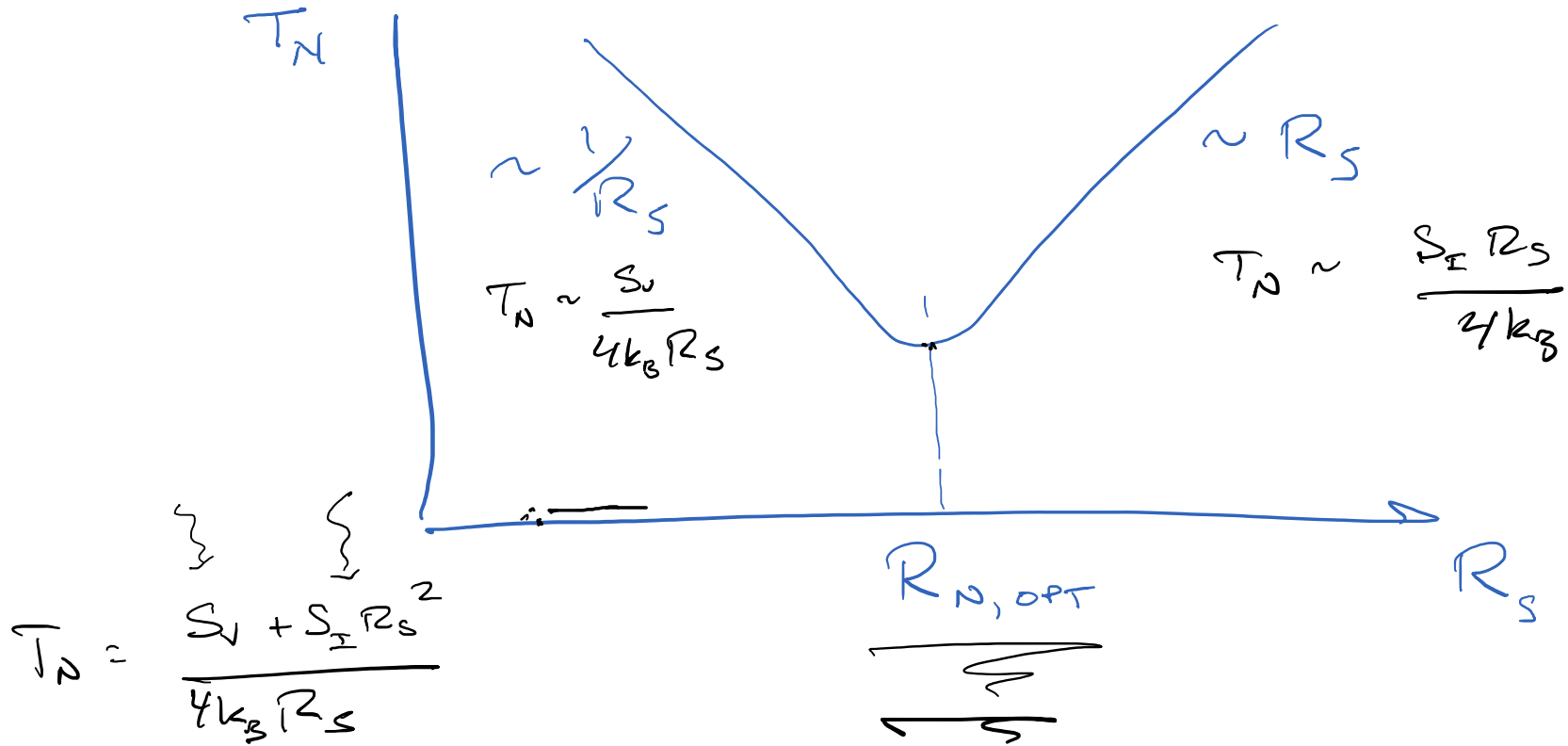
AMP CONTRIBUTION TO NOISE :

$$\rightarrow S_v + S_i R_s^2$$

AMP NOISE TEMPERATURE :

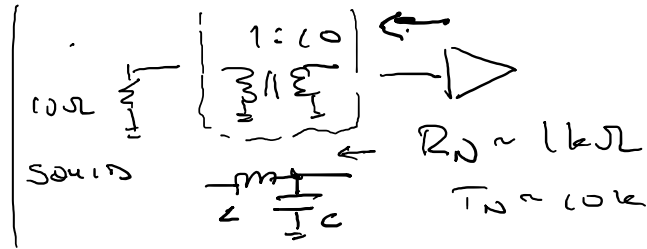
$$T_N = \frac{S_v + S_i R_s^2}{4k_B R_s}$$

# DEPENDENCE ON SOURCE RESISTANCE





$$T_N = \frac{S_V + S_I R^2}{4kR}$$



$$\frac{dT_N}{dR} = 0 \Rightarrow -\frac{S_V}{R^2} + \frac{S_I}{R} = 0$$

$$\Rightarrow R_{N,OPT} = \sqrt{\frac{S_V}{S_I}}$$

→ OPTIMAL SOURCE RESISTANCE

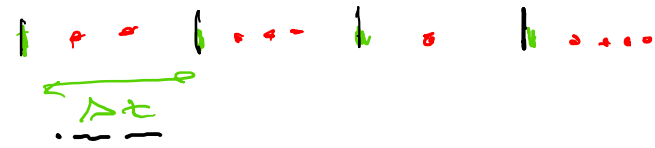
FOR LOW ADDED AMPLIFIER NOISE

NOISE AMPLITUDE

$$\begin{array}{l} \underline{e_n \text{ OR } v_n} \rightarrow \frac{nV}{\sqrt{Hz}} \\ \underline{i_n} \rightarrow \frac{pA}{\sqrt{Hz}} \end{array} \quad R_{N,OPT} = \frac{e_n}{i_n}$$

# OTHER NOISE PROCESSES

SHOT NOISE  $S_I = 2eI \Rightarrow$  DUE TO DISCRETENESS OF CHARGE



POISSON STATISTICS

→ MEAN-SQUARE CURRENT FLUCTUATION

$$\langle \delta I^2 \rangle = \frac{Ne^2}{\Delta t^2} = \frac{Ie}{\Delta t}$$

$N \rightarrow$  MEAN # OF CHARGES PER INTERVAL.

$$I = \frac{Ne}{\Delta t}$$

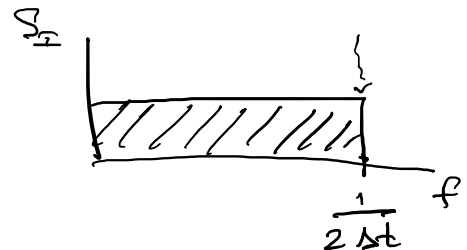
But

$$\langle \delta I^2 \rangle = S_I \frac{1}{2\Delta t}$$

NYQUIST FREQUENCY

$$\langle \delta I^2 \rangle = \int S_I df$$

$$S_I = 2eI$$



# TELEGRAPH NOISE



TWO-STATE SYSTEM

MEAN DWELL TIME  $\tau$

$$\text{power, } S(f) = \int \langle v(t)v(0) \rangle e^{-2\pi f t} dt$$

$$\langle v(t)v(0) \rangle = +1 \cdot P(\text{EVEN}) - 1 \cdot P(\text{ODD})$$

$$P_n(\lambda, t) = e^{-\lambda} \frac{\lambda^n}{n!}$$

$$\langle v(t)v(0) \rangle = e^{-\lambda} \left\{ \sum_{\substack{n \\ \text{EVEN}}} \frac{\lambda^n}{n!} - \sum_{\substack{n \\ \text{ODD}}} \frac{\lambda^n}{n!} \right\} = e^{-2\lambda}$$

$$\lambda = \tau / \alpha$$

$$\therefore \langle v(t) v(0) \rangle = e^{-2t/\alpha}$$

$$S(f) = \int e^{-2t/\alpha} e^{-2\pi j f t} dt$$

$$S(f) = \frac{\tau}{1 + 4(2\pi f \tau)^2}$$

